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AN ANALYSIS OF ACCURACY OF A PROCEDURE FOR COMPUTING LOWER CONFIDENCE LIMIT ON SYSTEM RELIABILITY UTILIZING SUBSYSTEM TEST DATA

by

Maurice Joseph Moran

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# UNITED STATES NAVAL POSTGRADUATE SCHOOL



### **THESIS**

AN ANALYSIS OF ACCURACY OF A PROCEDURE FOR COMPUTING LOWER CONFIDENCE LIMIT ON SYSTEM RELIABILITY UTILIZING SUBSYSTEM TEST DATA

bу

Maurice Joseph Moran

DECEMBER 1968

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#### AN ANALYSIS OF ACCURACY OF A PROCEDURE FOR COMPUTING

#### LOWER CONFIDENCE LIMIT ON SYSTEM RELIABILITY

UTILIZING SUBSYSTEM TEST DATA

Ъу

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Submitted in partial fulfillment of the requirements for the degree of

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#### ABSTRACT

Systems which are composed of two or more phases, or subsystems, arranged in logical sequence are found frequently in industry and defense. Standard procedures for computing lower confidence limits on reliability of such systems rely on the use of system data.

Engineering changes to any of these subsystems can effect the invalidation of all existing data, necessitating additional, sometimes extensive, testing. Such changes are not infrequent in complex systems. A need exists for a method of computing lower confidence limits on reliability which uses phase data. Some approximation techniques have become available. One such technique is currently being used by Applied Physics Laboratory, The Johns Hopkins University. Computer simulation techniques are used to analyze the accuracy of this procedure.

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#### CHAPTER I

#### INTRODUCTION

Current technology has produced a class of systems which are composed of two or more phases, or subsystems, arranged in logical sequence, such that the success of the system depends upon the success of the component phases. Thus the reliability of the system,  $R_{\rm s}$ , depends upon the reliability of each of the k phases of which it is composed. We express this mathematically as follows:

$$R_{s} = \prod_{i=1}^{k} R_{i}$$
 (1)

where R<sub>i</sub> is the reliability of the i<sup>th</sup> phase. Standard statistical procedures used to compute lower confidence limits (LCL) on R<sub>s</sub> require the use of system test data. Whenever high degrees of reliability, at high confidence levels, are demanded of a system, extensive testing is required, frequently at considerable cost.

Engineering changes to any one of the phases may cause the invalidation of all previous system test data. There is a need for a procedure to construct lower confidence limits on system reliability using phase test data which will salvage as much of the data as possible.

Approximation procedures are becoming available for so constructing these LCL's, one of which is currently being used by Applied Physics Laboratory, The Johns Hopkins University. This procedure is discussed in [1].

The purpose of this paper is to analyze the accuracy of this procedure. Computer simulation techniques will be used to accomplish this analysis.

<sup>&</sup>lt;sup>1</sup>Numbers in brackets refer to items in the bibliography with the same number.

#### CHAPTER II

#### COMPUTATIONAL PROCEDURE EMPLOYED BY APPLIED PHYSICS LABORATORY

The APL method for constructing LCL's on  $R_{\rm S}$  assumes the following:

- a) mutually independent trials
- b) the distribution of the reliability estimator,  $\hat{R}_{\text{S}}$ , is normal.

The formula for computing the  $100(1-\alpha)\%$ , one-sided LCL,  $\hat{R}_L$ , is

$$\hat{R}_{L} = \hat{R}_{S} - P(1-\alpha) \cdot \hat{\sigma}_{\hat{R}_{S}}$$
 (2)

where  $\hat{R}_{_{\bf S}}$  is the system reliability estimator,  $P(1-\alpha)$  is the  $100(1-\alpha)$  percentile of the standard normal distribution, and  $\hat{\sigma}_{\hat{R}}$  is the standard deviation estimator for the  $\hat{R}_{_{\bf S}}$  distribution

$$\hat{R}_{S} = \prod_{i=1}^{k} \hat{R}_{i}$$
(3)

where  $\hat{R}_{i}$  is the phase reliability estimator and is defined by

$$\hat{R}_{i} = s_{i}/n_{i} . \tag{4}$$

That is,  $\hat{R}_i$  denotes the proportion of successes for the i<sup>th</sup> phase,  $s_i$ , out of  $n_i$  trials.

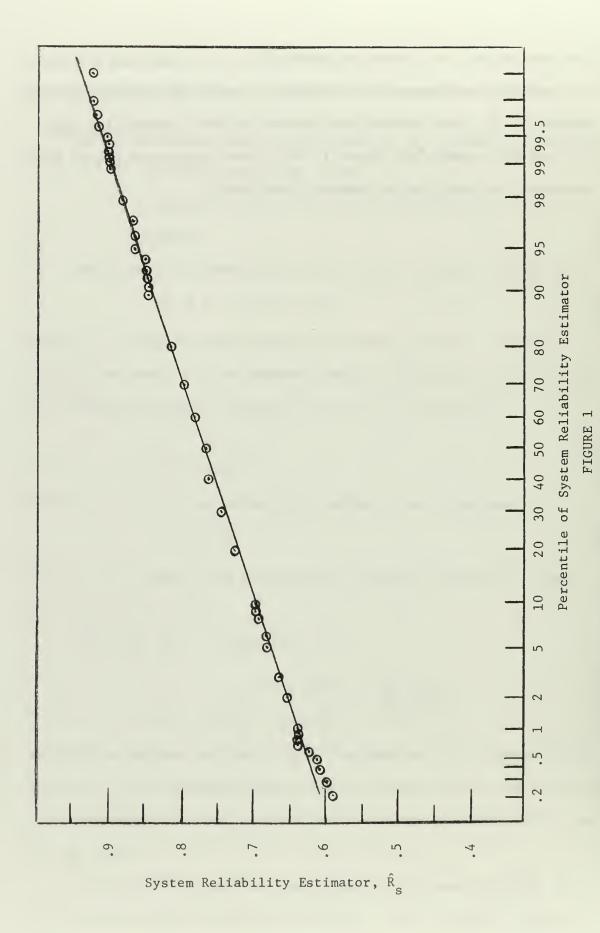
The value  $\hat{\sigma}_{\hat{R}_{_{\mathbf{S}}}}$  is computed by

$$\hat{\sigma}_{\hat{R}}^{2} = \prod_{i=1}^{k} \hat{R}_{i} - \prod_{i=1}^{k} \left[ \hat{R}_{i} - \frac{\hat{R}_{i}(1-\hat{R}_{i})}{n_{i}-1} \right]$$
 (5)

which is an unbiased estimator of the variance of  $\hat{R}_s$ . Standard deviation,  $\hat{\sigma}_{\hat{R}_s}$ , is obtained by extracting the square root of the variance. Although biased, this estimator is considered to be sufficiently close to  $\sigma_{\hat{R}_s}$  [1].

As stated above, one basic assumption of the model is that  $\hat{R}_{_{\mbox{S}}}$  is a normally distributed random variable. As an ancillary result of

the simulation, this assumption was verified for those cases for which the procedure was reasonably accurate. For each case considered, 1000 values of  $\hat{R}_{_{\rm S}}$  were computed and plotted on normal probability paper. For one such example see Figure 1. For those cases which proved less accurate, the distribution departed from normal.



ONE EXAMPLE OF THE NORMAL DISTRIBUTION OF SYSTEM RELIABILITY ESTIMATOR (CASE 32, TABLE II)

-8-

#### CHAPTER III

#### THEORY OF THE SIMULATION TECHNIQUE

One standard interpretation which can be applied to the meaning of a lower confidence limit involves the method used to compute it. This says that regardless of the true value of  $R_{_{\rm S}}$  the computation will produce an LCL,  $\hat{R}_{_{\rm L}}$ , which is less than  $R_{_{\rm S}}$  (1- $\alpha$ )% of the time. Use can be made of this interpretation in formulating the simulation model.

If one were to use an exact method of determining  $\hat{R}_L$  and repeated the process several times, he could expect that approximately  $(1-\alpha)$ % of the values would be less than  $R_s$ . As the number of replications approaches infinity, he could expect that exactly  $(1-\alpha)$ % of the values would be less than  $R_s$ .

One could use a similar approach to evaluate the accuracy of an unproven method. Given a hypothetical system of known  $R_{\rm i}$ , and hence known  $R_{\rm s}$ , one could use the proposed method to compute  $\hat{R}_{\rm L}$  on  $R_{\rm s}$ . If the method was accurate, approximately  $(1-\alpha)\%$  of the values so computed would be less than  $R_{\rm s}$ . If the number of replications was sufficiently large, the percentile of  $\hat{R}_{\rm L}$  which is less than  $R_{\rm s}$  would be a good measure of the accuracy of the procedure. This percentile will be denoted  $A_{1-\alpha}$ 

The computer simulation technique, used herein, follows the above approach. The rapid computational ability of the computer allows one to simulate the testing process, compute  $\hat{R}_L$ , and replicate the process a great many times. One of our measures of effectivess of the method will be the relative closeness of  $A_{1-\alpha}$  to  $R_s$ . Other measures of effectiveness will be discussed in the results section of this paper.

The simulation technique begins by reading from data the parameters of the case to be considered; i.e., KK, the number of replications desired (1000 for all cases considered herein); K, the number of phases per system;  $\mathbf{R_i}$  and  $\mathbf{n_i}$  for all phases; and  $\alpha.$  Using a pseudo-random number generator and the known phase reliabilities, test data is gathered on each of the phases by comparing  $\mathbf{n_i}$  random numbers with  $\mathbf{R_i}$  (i = 1, 2, ..., K). Each time the random number generator produces a number less than or equal to  $\mathbf{R_i}$  it is counted as a successful test. A running total of successes,  $\mathbf{s_i}$ , is kept throughout the course of testing. After having so obtained these data, SUBROUTINE RHAT is called with parameter  $\alpha$ . The values  $\mathbf{s_i}$  and  $\mathbf{n_i}$  are made available to RHAT via the DIMENSION statement. SUBROUTINE RHAT returns the values  $\hat{\mathbf{R}_L}$  and  $\hat{\mathbf{R}_S}$ . This operation is repeated for KK replications to compute KK values of  $\hat{\mathbf{R}_L}$  and  $\hat{\mathbf{R}_S}$ . These values are stored in vector matrices for later use.

SUBROUTINE RHAT is a relatively straightforward application of the working formulae contained in Chapter 2. One point worthy of note is that only ten values of  $P(1-\alpha)$  have been read into computer memory in order to conserve memory space. The argument  $(1-\alpha)$  is digitized to facilitate stowage and retrieval. This limits the values of  $\alpha$  which can be used to increments of .05, from .05 to and including .50, a limitation which can easily be changed as the requirements dictate.

<sup>&</sup>lt;sup>2</sup>The pseudo-random number generator used herein is a library sub-routine of the Computer Facility, Naval Postgraduate School, Monterey. A printout of this subroutine is included in Appendix II.

<sup>&</sup>lt;sup>3</sup>The reader is invited to follow the program logic by referring to Appendix II. Extensive use is made of comment cards to explain the operations as they are accomplished. The program notation is intended to be the same in meaning as that of the body of the paper. It is, of necessity, somewhat different in form because of machine limitations. As an aid, a glossary of terms is provided in Appendix I.

As the above values of  $\,\hat{R}_L^{}$  are generated, they are summed for eventual division by KK to compute their mean.

Thus far, the simulation has performed the following operations:

- 1) generated the statistics  $s_i$  (i = 1, 2, 3, ..., K)
- 2) computed the values for the  $\hat{R}_s$ ,  $\hat{R}_L$  and Al matrices (Al being an exact duplication of the  $\hat{R}_L$  matrix)
- 3) summed the values of  $\,\hat{R}_L^{}\,$  to get the mean,  $\,\mu_{\hat{R}_T^{}}^{}\,$  .

Next, a sorting routine, SUBROUTINE SHSORT, 4 is called for the purpose of putting matrices  $\hat{R}_S$  and Al into ascending numerical order. This is done to facilitate plotting these values on probability graph paper to determine their distributions. This also facilitates obtaining the  $100(1-\alpha)$  percentile of the  $\hat{R}_L$  distribution,  $A_{1-\alpha}$ . Recall the matrix Al was identical to the matrix  $\hat{R}_L$  before it was ordered. Thus,  $A_{1-\alpha}$  equals the KK(1- $\alpha$ ) th member of the ordered Al matrix.

Next, the percentile of  $\hat{R}_L$  which is less than  $R_s$  is obtained; i.e., the probability  $\hat{R}_L$  is less than  $R_s$ , denoted  $P(R_s)$ . This is computed by determining the last element of the ordered Al matrix whose value is less than or equal to  $R_s$  and dividing its index number by KK.

The variance of  $\hat{R}_L$ ,  $\sigma_{\hat{R}_L^2}$ , is calculated next by summing the squared differences of  $\hat{R}_L$  and  $\mu_{\hat{R}_L}$  and dividing by KK, the number of replications,

$$\sum_{\underline{i}=1}^{KK} (\hat{R}_{\underline{l}} - \mu_{\hat{R}_{\underline{l}}})$$

 $<sup>^4{</sup>m This}$  subroutine is a library subroutine of the Computer Facility, Naval Postgraduate School, Monterey, Calif. It is printed out in Appendix II.

The square root is later extracted to obtain the standard deviation,  ${}^\sigma\hat{R}_L$ 

The difference between  $\,R_{_{\rm S}}\,$  and  $\,A_{_{\rm 1-}\alpha}\,$  is then obtained, which is the primary measure of effectiveness of the procedure.

The remaining statements are editorial in nature; e.g., input/output statements which read in data or printout results. Others initialize variables, sums, or products to ensure that values are not carried over from replication to replication.

The program output may be summarized as follows:

- a) 1000 values of system reliability estimator,  $\hat{R}_{_{\mbox{\scriptsize S}}},$  in ascending numerical order
- b) 1000 values of LCL,  $\hat{R}_{T}$ , in chronological order
- c) 1000 values of LCL,  $\hat{R}_{L}$ , in ascending numerical order
- d) system reliability, R<sub>s</sub>
- e) 100(1- $\alpha$ ) percentile of the population of  $\hat{R}_L$  population,  ${}^A_{1-\alpha}$
- f) standard deviation of  $\hat{R}_L$  population,  $\sigma_{\hat{R}_L}$
- g) probability that  $\hat{R}_L$  is less than  $R_S$ ,  $P(R_S)$
- h) mean of  $\hat{R}_L$ ,  $\mu_{\hat{R}_T}$
- i) the difference between  $R_{\rm S}$  and  $A_{1-\alpha}$
- j)  $\Sigma n_i q_i$ , a measure of the amount of testing done and the unreliability  $(q_i)$ , or failure rate

#### CHAPTER IV

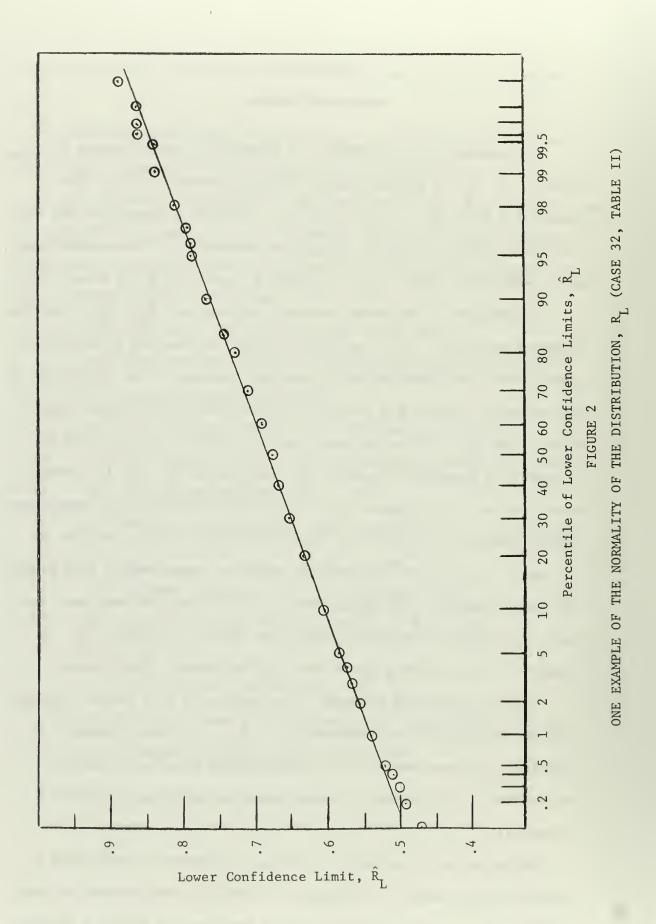
#### SIMULATION RESULTS

The accuracy of the procedure is measured by the closeness of  $A_{1-\alpha}$  relative to  $R_s$ . A second measure of effectiveness,  $P(R_s)$ , the probability that  $\hat{R}_L$  is less than  $R_s$ , provides a measure of the true confidence level achieved by using this procedure. If the method were exact, one could expect  $A_{1-\alpha}$  to equal  $R_s$  and  $P(R_s)$  to equal  $(1-\alpha)$ .

In addition to the above criteria, the mean of  $\hat{R}_L$ ,  $\mu_{\hat{R}_L}$ , and the standard deviation,  $\sigma_{\hat{R}_L}$ , are also provided as measures of effectiveness. These two characteristics provide a measure of the likelihood of the procedure producing a lower confidence limit which differs considerably from  $R_S$ . It can be shown that for those cases for which the procedure is reasonably accurate the distribution of  $\hat{R}_L$  is approximately normal. (See Figure 2.) Thus if the procedure is accurate, one should expect to find the 1- $\alpha$  percentile to be a known function of the mean; e.g., the 90<sup>th</sup> percentile should be approximately 1.28 standard deviations above the sample mean. In addition, the mean and variance can be used to construct prediction regions into which  $\hat{R}_L$  is likely to fall, assuming again that  $\hat{R}_L$  is normally distributed.

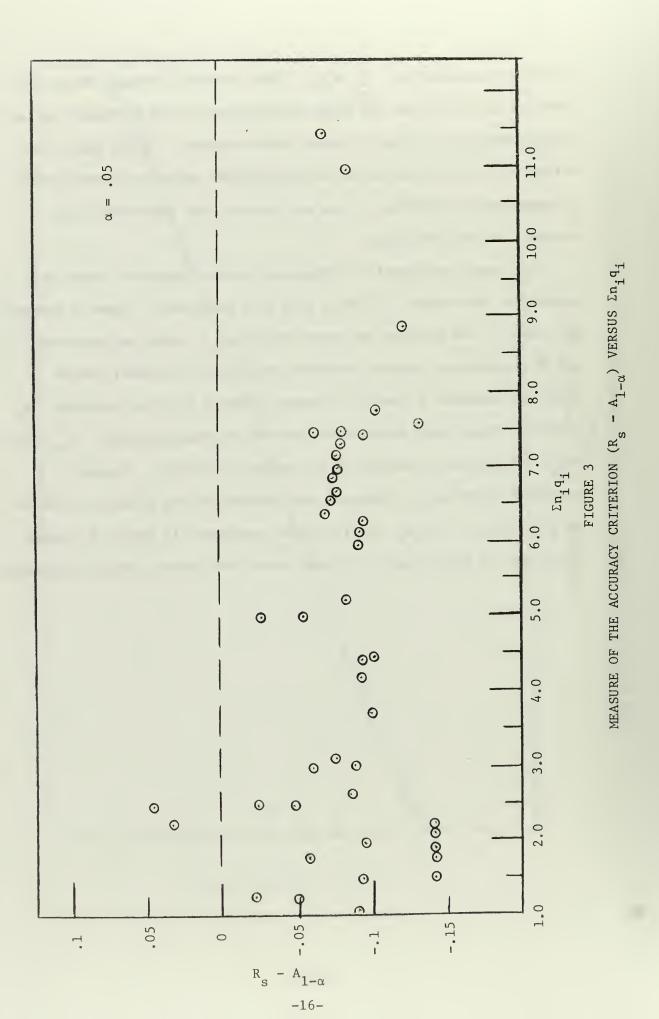
Several cases were examined in evaluation of this method. In each case one or more of the parameters, K,  $R_{i}$ ,  $n_{i}$ , were changed. In addition, each case was run for  $\alpha$ -values equal to .05, .1, and .2, successively. The results of these cases are tabulated in Tables I through III.

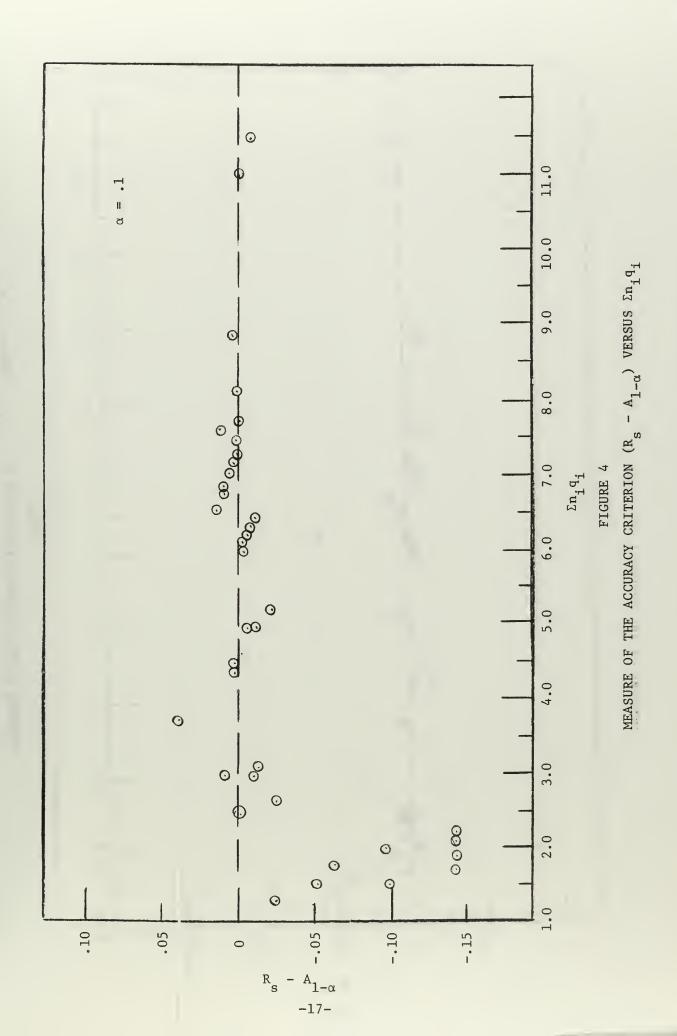
The accuracy of reliability testing procedures is most often a function of the amount of testing,  $\mathbf{n_i}$ , and the unreliability of the subsystems,  $\mathbf{q_i}$ . This quantity is also tabulated in Tables I through

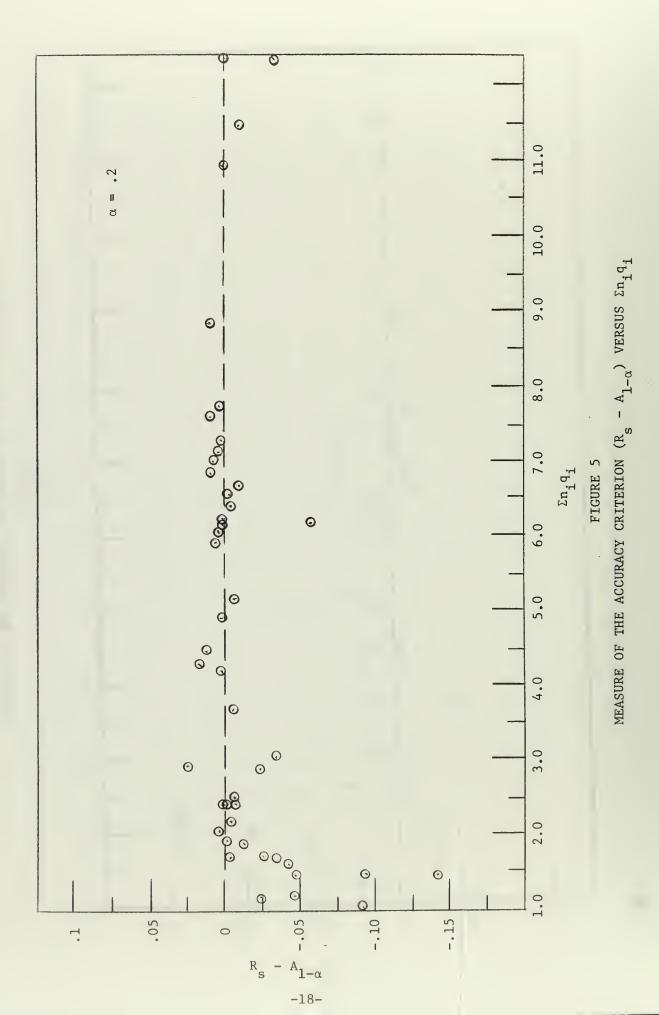


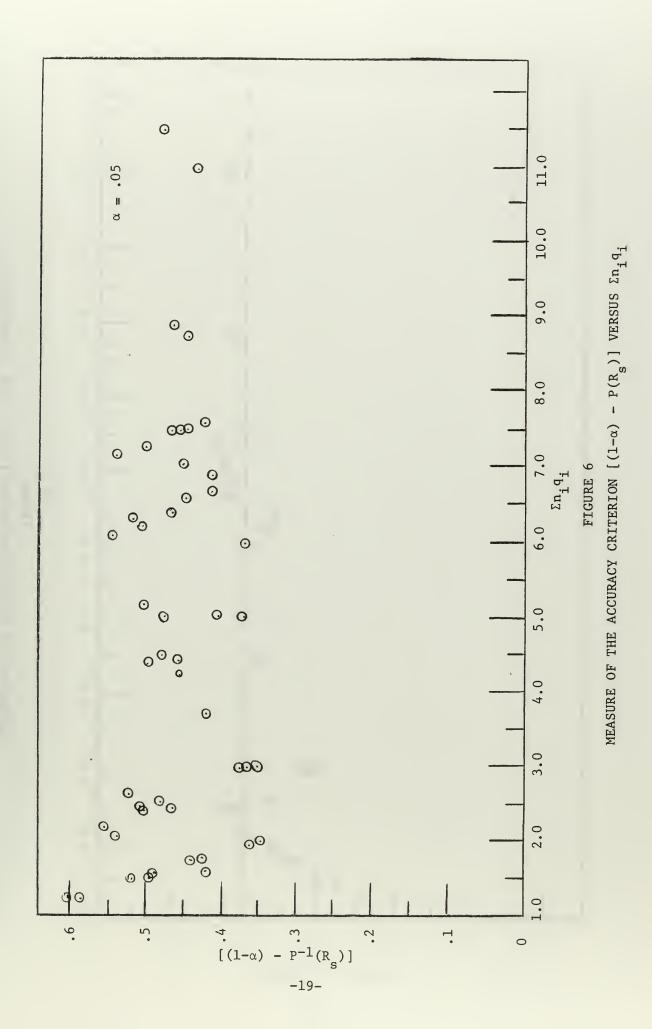
III and is expressed by  $\sum\limits_{i=1}^{K} n_i q_i$ . Thus Tables I through III provide criteria upon which one can judge the accuracy of the procedure and an effective measure of when to expect this accuracy. If one knows the reliabilities for which he is striving and the amount of testing which is economically feasible, he has available a good estimate of the accuracy of this procedure.

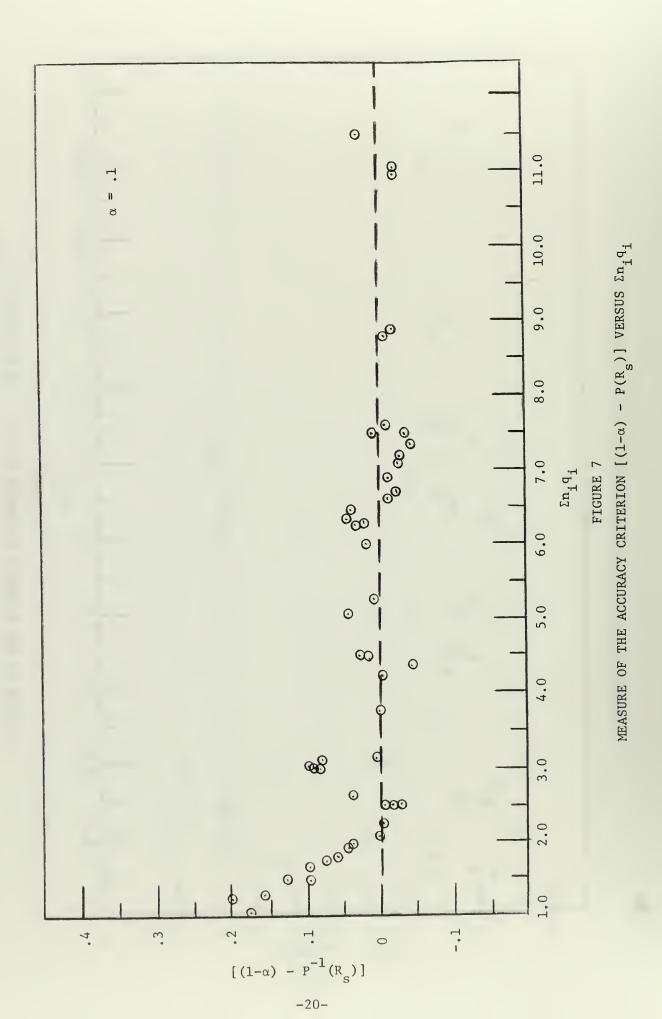
The cases considered are tabulated in three separate tables according to the purpose for which they were considered. Cases 1 through 24, Table I, are the same as those considered by Woods and Borsting [2] and are intended to provide a direct comparison with their method. Table III contains a "family" of cases in which only the parameter  $\mathbf{n}_i$  changes. These cases demonstrate how the accuracy criteria,  $\mathbf{A}_{1-\alpha}$  and  $\mathbf{P}(\mathbf{R}_s)$ , behave as a function of the amount of testing. Figures 3 through 8 graphically illustrate the behavior of the accuracy criteria as a function of  $\Sigma \mathbf{n}_i \mathbf{q}_i$  for the cases considered in Tables I through III. Each of these graphs utilizes one of the three  $\alpha$ -levels considered.











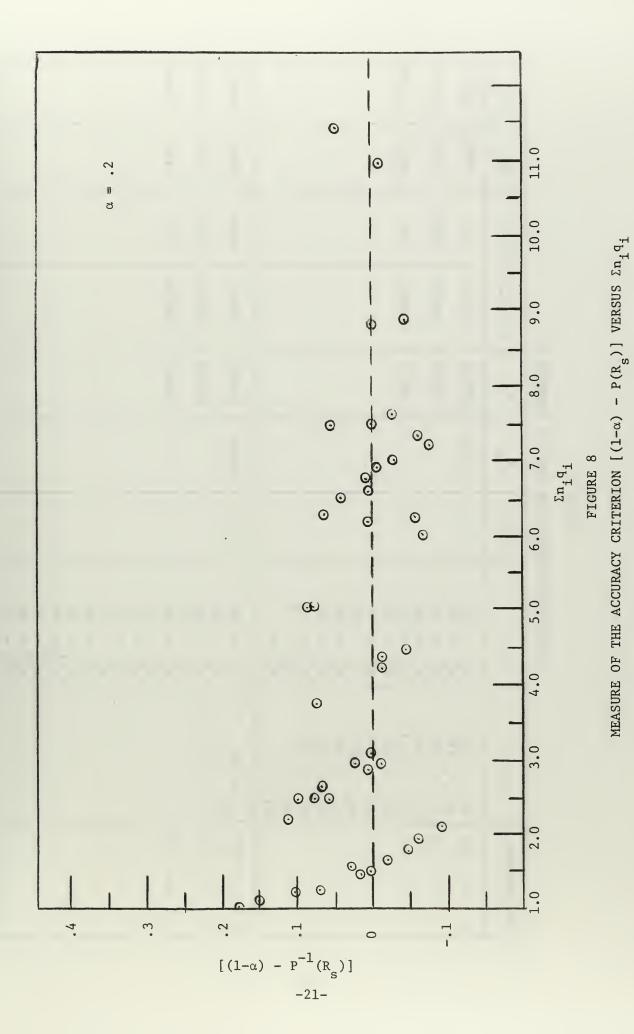


TABLE I

SIMULATION RESULTS FOR CASES 1 THROUGH 24

O R.	.1227	.05014
μ Ř Ĺ	.59045	.85872
P(R)	.89300	.4680
R -A <sub>1-α</sub>	13811 00448 01048	07427
$A_{1-\alpha}$	.72779	.86759
	.72331	.86006
Σniqi	15.43	11.55
$\mathbf{n_i}$ $\Sigma \mathbf{n_i} \mathbf{q_i}$ $\mathbf{R}$	n = 150 n = 150 n = 90 n = 90 n = 100 n = 125 n = 125 n = 125 n = 63 n = 63 n = 63 n = 63 n = 63 n = 125 n	n n2 = 250 n3 = 120 n4 = 120 n5 = 65 n6 = 70 n7 = 70 n9 = 90 n10 = 60 n11 = 60 n12 = 20 n13 = 20 n14 = 30 n15 = 30
q,	q <sub>1</sub> = .005 q <sub>2</sub> = .015 q <sub>4</sub> = .012 q <sub>5</sub> = .012 q <sub>6</sub> = .02 q <sub>7</sub> = .003 q <sub>8</sub> = .005 q <sub>10</sub> = .005 q <sub>11</sub> = .005 q <sub>11</sub> = .005 q <sub>12</sub> = .03	q <sub>i</sub> = .01 i = 1,2,,15
CASE NUMBER	$1  \alpha = .05$ $\alpha = .10$ $\alpha = .20$	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$

Table I (continued)

CASE NUMBER	q <u>i</u>	n 1	Σn <sub>i</sub> q <sub>i</sub>	S S	$A_{1-\alpha}$	$R_s-A_{1-\alpha}$	P(R <sub>S</sub> )	r, L	G, L
$3  \alpha = .05$	q <sub>1</sub> = .005	$n_1 = 20$	4.40	.79239	.950	15761	.4540	.79305	.08963
$\alpha = .10$	i = 1,2,14	i = 1,2,,15			.79207	.00032	.9430	.65585	.11241
α = .20	q <sub>15</sub> = .15				.77636	.01604	.8160	.70426	.10391
$4  \alpha = .05$	q <sub>1</sub> = .005	$n_1 = 40$	8.80	.79239	006.	10761	.5020	.79439	79090
$\alpha = .10$	i = 1,2,,14	i = 1,2,,15			.79205	.00035	.9140	.69402	.07415
$\alpha = .20$	q <sub>15</sub> = .15				.79493	00254	.7950	.73159	.06922
$5  \alpha = .05$	q <sub>1</sub> = .005	n <sub>j</sub> = 50	11.00	.79239	.88357	09117	.5160	.7893	.05816
$\alpha = .10$	i = 1,2,,14	i = 1,2,,15			.78521	.00718	.9250	.70359	.0637
$\alpha = .20$	q <sub>15</sub> = .15				.78932	.00308	0608.	.73802	.0587
9 α = .05	q <sub>1</sub> = .005	$n_1 = 100$	22.0	.72939	.85675	06435	.5060	.79237	.03993
$\alpha = .10$	i = 1,2,,14	i = 1,2,,15			.78657	.00582	.92900	.72918	.04313
$\alpha = .20$	q <sub>15</sub> = .15				.78563	92900.	.8420	.74834	.04367
$7  \alpha = .05$	q <sub>j</sub> = .005	n; = 150	7.65	.79239	.92479	1324	.5220	.78733	.0840
$\alpha = .10$	i = 1,2,,14	i = 1,2,,5			.78111	.01129	.9110	.66055	.1068
α = .20	q <sub>15</sub> = .15	$n_1 = 20$			96662.	00756	.7740	.70772	.10288
		- 1							
8 α = .05	q <sub>1</sub> = .005	$n_1 = 20$	23.90	.79239	.880	08761	.48400	.79330	.05387
$\alpha = .10$	i = 1,2,,14	i = 1,2,,14			.81324	02084	.8430	.70764	.07529
α = .2	q <sub>15</sub> = .15	$n_{15} = 150$			.80882	01643	.7380	.74255	.07156

Table. I (continued)

σ̂,	.03007	.04063 .05526 .04817	.04632	.03992 .0444 .04158	.06307 .09101 .08276	.05885
<sup>µ</sup> Ř,	.95076 .90733 .92093	.90414 .83963 .86752	.85961 .78163 .81401	.77327 .70770 .73251	.88114 .78420 .82409	.88176 .81133 .83840
P(R <sub>S</sub> )	.46500 .9090 .7290	.5680 .8580 .71800	. 9000	.5380 .9390 .8210	.3720 .8200 .79700	.440 .86900 .7420
$R_s-A_{1-\alpha}$	04901 .00389 00825	05602 01043 00228	08113 .00028 00106	06662 .01080	07778 01198 03626	05897 00476 00108
$^{A_{1-\alpha}}$	1.000 .94710 .95924	.96040 .91481 .90666	.94119	.84040 .76298 .76706	.960 .89420 .91848	.94119
S.	.95099	.90438	90098.	.77378	.88222	.88222
Σniqi	2.5	5.0	7.5	25.0	3.125	6.25
n i	n <sub>1</sub> = 50 i = 1,2,,5	$n_1 = 50$ i = 1,2,,10	n <sub>1</sub> = 50 i = 1,2,,15	n <sub>1</sub> = 100 i = 1,2,,5	n <sub>1</sub> = 25 i = 1,2,,25	n <sub>1</sub> = 50 i = 1,2,,25
q <sub>i</sub>	q <sub>i</sub> = .01 i = 1,2,,5	q <sub>i</sub> = .01 i = 1,2,,10	q <sub>i</sub> = .01 i = 1,2,,15	q <sub>i</sub> = .05 i = 1,2,,5	q <sub>i</sub> = .005 i = 1,2,,25	q <sub>i</sub> = .005 i = 1,2,,25
CASE NUMBER	9 α = .05 α = .10 α = .20	10 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	11 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	12 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	13 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	14 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$

Table I (continued)

s)   "R, GR,	.88219	00 .83130 .03493 700 .85177 .03467	30 .65253 .09817 50 .70017 .08446	70 .77843 .05719 0 .6880 .05889 70 .72433 .05934	70 .60624 .08947 30 .46388 .08305 40 .51687 .09016	) .95638 .05440 70 .94434 .06557 00 .97502 .03063	,97593 .02104
$R_{s}-A_{1-\alpha}$ P(R <sub>s</sub> )		.00342 .9400 00232 .77700	10643 .440 00148 .8730 .00234 .8660	08982 .4870 .01042 .940 00205 .7770	14568 .4870 .02930 .9400 .03151 .8640	02470 .430 02470 .4470 02470 .4700	02470 .347
$A_{1-\alpha}$	.93206	.87880	.88474 .77979 .77597	.86813 .76789 .78036	.75145	1.000	1.000
M <sub>S</sub>	.88222		.77831	.77831	.60577	.97530	.97530
Σniqi	12.50		6.25	12.50	12.50	.6250	1.250
n	i = 100	i = 1,2,,25	n <sub>1</sub> = 25 i = 1,2,,50	n <sub>1</sub> = 50 i = 1,2,,50	$n_1 = 25$ i = 1,2,,100	n <sub>i</sub> = 25 i = 1,2,,25	$n_{\mathbf{j}} = 50$
q.	q <sub>1</sub> = .005	i = 1,2,,25	q <sub>i</sub> = .005 i = 1,2,,50	q <sub>i</sub> = .005 i = 1,2,,50	q <sub>i</sub> = .005 i = 1,2,,100	q <sub>i</sub> = .001 i = 1,2,,25	$q_{1} = .001$
CASE NUMBER	Ш	α = .10	16 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	17 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	18 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	19 α = .05 α = .10 α = .20	20 α <sub>c</sub> = .05

Table I. (continued)

OR,	.01576	.04112	.03073	.05847
μ <sub>Ř</sub> ,	.97551 .95206 .9603	.95244 .89353 .91708	.95171 .90579	.90578 .81775
P(R <sub>S</sub> )	.92100	.7020	.4440 .92100 .7070	.9210
R -A <sub>1-α</sub>	.02470	04880 04880 04880	04880 .00410 00804	09522 .01059 01369
$A_{1-\alpha}$	1.000 .97355 .97962	1.000	1.000 .94710 .95924	1.000 .89420 .91848
R S	.97530	.95120	.95120	.90478
$\Sigma_{\mathbf{n_i}} \mathbf{q_i}$	2.50	1.250	2.50	2.50
n 1	n <sub>1</sub> = 100 i = 1,2,,25	n <sub>i</sub> = 25 i = 1,2,,50	n <sub>i</sub> = 50 i = 1,2,,50	n <sub>1</sub> = 25 i = 1,2,,100
q <sub>1</sub>	q <sub>i</sub> = .001 i = 1,2,,25	q <sub>i</sub> = .001 i = 1,2,,50	q <sub>i</sub> = .001 i = 1,2,,50	q <sub>i</sub> = .001 i = 1,2,,100
CASE NUMBER	21 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	22 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	23 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	24 α = .05 α = .10 α = .20

TABLE II

SIMULATION RESULTS FOR CASES 25 THROUGH 51

.05 .04 .1 .1 .05 .05 .03 .03 .03		q,	n,	Σniqi	R	Α1-α	$R_s-A_{1-\alpha}$	P(R <sub>S</sub> )	<sup>L</sup> Ř.	°Ř.
= 26       .86531       .00109       .9090         = 23       .86368       .00272       .8180         = 40       8.90       .7290       .85598      12698       .4800         = 26       .72340       .0056       .9200         = 40       4.45       .85737       .95652      09915       .4920         = 26       .86424      00687       .8850         = 26       .86424      00458       .7880         = 23       .86195      00458       .7880         = 26       .93387      0212       .8600         = 26       .93387      0212       .8600         = 26       .93387      0212       .8600         = 24       .92161      00894       .74200         = 25       .94119       1.0000      05881       .5080         = 26       .94905      05881       .82700         = 23       .94905      00786       .72800	$q_1 = .05$		11	4.27	7998.	.96154	09514	0067.	.86517	.06186
= 23       .86368       .00272       .8180         = 40       8.90       .7290       .85598      12698       .4800         = 26       .72340       .0056       .9200         = 40       4.45       .85737       .95652      09915       .4920         = 40       4.45       .85737       .95652      09915       .7880         = 40       2.670       .91267       1.000      08733       .4270         = 26       .91267       1.000      08733       .4270         = 26       .93387      0212       .8600         = 26       .94119       1.0000      05881       .5080         = 40       1.780       .94119       1.0000      05881       .82700         = 26       2.670       .94119       1.0000      05881       .82700	$q_2 = .05$		11			.86531	.00109	0606.	.76788	99480°
= 40       8.90       .7290       .85598      12698       .4800         = 26       .72340       .0056       .9200         = 40       4.45       .85737       .95652      09915       .4920         = 40       4.445       .85737       .95652      09915       .4920         = 26       .86424      00687       .8850         = 40       2.670       .91267       1.000      08733       .4270         = 26       .93387      0212       .8600         = 23       .94119       1.0000      05881       .5080         = 40       1.780       .94119       1.0000      05881       .5080         = 26       1.0000      05881       .82700         = 26       2.670       .94119       1.0000      05881       .72800	43 = °04		П			.86368	.00272	.8180	.80288	.07501
= 26       .72340       .0056       .9200         = 23       .71984       .00916       .8410         = 40       4.45       .85737       .95652      09915       .4920         = 26       .86424      00687       .8850         = 40       2.670       .91267       1.000      08733       .4270         = 26       .93387      0212       .8600         = 26       .93387      0212       .8600         = 240       .94119       1.0000      08733       .74200         = 25       .94119       1.0000      05881       .5080         = 26       .94905      00786       .72800	q <sub>1</sub> = .1		II	8.90	.7290	.85598	12698	.4800	.73319	90220.
= 23       .71984       .00916       .8410         = 40       4.45       .85737       .95652      09915       .4920         = 26       .86424      00687       .8850         = 40       2.670       .91267       1.000      08733       .4270         = 26       .93387      0212       .8600         = 23       .92161      00894       .74200         = 26       .94119       1.0000      05881       .5080         = 26       .94905      05881       .82700         = 23       .94905      00786       .72800	$q_2 = .1$		II			.72340	9500.	.9200	.60014	.0924
= 40       4.45       .85737       .95652      09915       .4920         = 26       .86424      00687       .8850         = 40       2.670       .91267       1.000      08733       .4270         = 26       .93387      0212       .8600         = 23       .92161      00894       .74200         = 40       1.780       .94119       1.0000      05881       .5080         = 26       1.0000      05881       .82700         = 23       23      00786       .72800	q <sub>3</sub> = .1		П			.71984	.00916	.8410	.64682	.08542
= 26 = 23 = 40 = 26 = 26 = 40 = 26 = 25 = 40 = 28 = 23 = 40 = 28 = 40 = 28 = 40 = 28 = 40 = 28 = 40 = 28 = 28	4 <sub>1</sub> = .05		II.	4.45	.85737	.95652	09915	.4920	.85785	.06459
= 23	q <sub>2</sub> = .05		П		erend-dominische	.86424	00687	.8850	.75173	.0888
= 40	II		II			.86195	00458	.7880	.79357	.07963
= 26 = 23 = 40 = 40 = 26 = 25 = 25 = 25 = 25 = 25 = 23 = 26 = 26 = 26 = 28 = 28	q <sub>1</sub> = .03		11	2.670	.91267	1.000	08733	.4270	.91452	.05062
= 23 .92161	II		11			.93387	0212	0098	.83343	.0802
= 40	II		11			.92161	00894	.74200	.86478	82690.
= 26 1.000005881 .82700 = 23 .9490500786 .72800	q <sub>1</sub> = .02		Ш	1.780	.94119	1.0000	05881	.5080	.94020	.04340
= 2300786 .72800	II		II			1.0000	05881	.82700	.87871	6220.
	q <sub>3</sub> = .02		II			.94905	00786	.72800	.89828	.06415

Table II (continued)

	q,	n,	Σn <sub>i</sub> q <sub>i</sub>	R S	Α1-α	$R_s-A_{1-\alpha}$	P(R <sub>S</sub> )	u Ř.	σ̂.
$q_1 = .01$ $q_2 = .01$		$n_1 = 40$ $n_2 = 26$ $n_3 = 26$	.8900	.97030	1.000	02970	.580	.93321	.03256
4 <sub>1</sub> = .05 1 = 1,2,	5,,5	n <sub>i</sub> = 30 i = 1,2,,5	7.500	.77378	.87310	09941 .00138	.4980	.65242	.07010
q <sub>i</sub> = .( i = 1,2	2,,5	n <sub>i</sub> = 50 i = 1,2,,5	12.50	.77378	.8666 .76514	09288 .00864 00245	.9480	.67909	.05771
$q_1 = .$ $i = 1,$	.05	$n_1 = 100$ i = 1,2,,5	25.0	.77378	.84030	06652 .01091	.5200	.77420	.03956
q <sub>i</sub> = , i = 1,	2,,5	n <sub>1</sub> = 30 i = 1,2,,5	1.50	.95099	1.000	04901 04901 04901	.4480	.94949	.03980
$q_1 = .$ $1 = 1,$	.01	n <sub>1</sub> = 50 i = 1,2,,5	2.50	.95099	1.000 .94710 .95924	04901 .00389 00825	.46700	.95068	.02950

Table II (continued)

Rs A <sub>1-α</sub> .95099 .98010 .95706
.97525 1.0000 1.0000 1.0000
.97525
.97525
.59874
.59874

Table II (continued)

or, L	.05318	.04032	.03699	.02893	.12615 .2875 .23079	.09327 .176 .150
r, L,	.90207 .82122 .85417	.90495	.95238 .89681	.95231 .90522 .92226	.90476	.90343 .78644 .82837
P(R <sub>S</sub> )	.8080	.5410	.42800 .7720 .76100	.4470 .9130 .72800	.3990 .3870	.6340 .6420 .62400
R -A <sub>1-α</sub>	06229 00745 02768	05602 01043 00228	04889	04889 .00401 00813	09608	09608 09608 09608
$A_{1-\alpha}$	.96667	.96040	1.000	1.0000	1.0000	1.0000
R S	. 90438	.90438	.95111	.95111	.90392	.90392
Σniqi	0	0	10	20		0
Σu	3.0	5.0	1.5	2.50	5.	1.0
n, Sn	$n_{i} = 30$ 3.0 i = 1,2,,10	n <sub>i</sub> = 50 i = 1,2,,10	n <sub>i</sub> = 30 1i = 1,2,,10	$n_1 = 50$ 2. i = 1,2,,10	$n_1 = 5$ .5	$n_1 = 10$ 1.0
	= 30 = 1,2,,10	= 50	= 30 = 1,2,,10	L = 50 = 1,2,,10	= 5	= 10

Table II (continued)

GR.	.07652	.06251	.05710	.05474
<sup>µ</sup> Ř.	.9025 .78892 .84026	.90542 .81014 .84586	.90320 .8157 .84959	.90397 .81856 .84915
P(R <sub>S</sub> )	.4510	.5990	.4790	.570 .8150
R -A <sub>1-α</sub>	09608 09608 09608	09608	09608 .00972 01456	06275
$A_{1-\alpha}$	1.0000	1.0000	1.0000	.96667
S S	. 90392	.90392	.90392	.90392
Σniqi	1.5	2.0	2.50	3.0
n	n; = 15 i = 1,2,,5	n <sub>i</sub> = 20 i = 1,2,,5	n <sub>i</sub> = 25 i = 1,2,,5	n <sub>1</sub> = 30 i = 1,2,,5
		2,5	5	5
q <sub>1</sub>	.05 q <sub>i</sub> = .02 .10 i = 1,2,.	$q_1 = .02$ $i = 1, 2,$	$q_1 = .02$ $i = 1,2,.$	$q_1 = .02$ i = 1,2,.

TABLE III

SIMULATION RESULTS FOR CASES 52 THROUGH 73

CASE NUMBER	q <sub>1</sub>	n,	Σniqi	R S	$A_{1-\alpha}$	$R_s-A_{1-\alpha}$	P(R <sub>S</sub> )	μ <sub>Ř</sub> ,	σ̂Ř
52 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	$q_1 = .05$ $i = 1,2,3$	$n_{i} = 5$ i = 1,2,3	.75	.85737	1.0000	14263 14263 14263	.5490	.85582 .66851 .74061	.15246 .3140 .25978
53 α = .05 α = .10 α = .20	q <sub>i</sub> = .05 i = 1,2,3	$n_{i} = 10$ i = 1,2,3	1.5	.85737	1.0000	14263 14263 14263	.4560	.86076 .70324 .76032	.10375
54 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	$q_1 = .05$ i = 1,2,3	$n_{i} = 11$ i = 1,2,3	1.65	.85737	1.0000 1.0000 .81473	14263 14263 .04265	.5240 .8060 .8260	.85370 .70654 .75394	.10233 .1780
55 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	$q_1 = .05$ i = 1,2,3	$n_1 = 12$ i = 1,2,3	1.80	.85737	1.0000	14263 14263 .02721	.51900 .84600 .84900	.86228 .71323 .76715	.09521 .1570 .13232
56 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	q <sub>i</sub> = .05 i = 1,2,3	$n_1 = 13$ i = 1,2,3	1.95	.85737	1.0000	14263 14263 .01414	.5840 .8590 .865	.85759 .71616 .77046	.09345 .1550

Table III (continued)

					Internation and story in a sec	
σ̂ <sub>L</sub>	.09187	.08831 .1342 .11535	.07924	.06624	.06071	.05628
μ <sub>Ř</sub>	.86265 .70868 .77051	.85663 .72411 .76565	.85636 .73029 .77710	.85884 .75165 .79207	.85908 .75990	.85615 .76684 .79653
P(R <sub>S</sub> )	.4060 .8910 .8910	.3860	.5120 .8220 .8180	.5260 .8990 .7250	.4660	.4410 .8930 .7930
$R_s-A_{1-\alpha}$	14263 14263 .00295	14263 .03370 00676	09263 .01038	10263 .03683 00788	10929 00213	08630 0200 00964
$A_{1-\alpha}$	1.0000 1.0000 .85443	1.0000 .82367 .86413	.9500 .86775 .83282	.9600 .89420 .86525	.96667 .85950	.94367 .87737 .86701
R	.85737	.85737	.85737	.85737	.85737	.85737
Σniqi	2.100	2.250	3.00	3.75	4.50	5.250
nj	$n_1 = 14$ i = 1,2,3	$n_1 = 15$ i = 1,2,3	$n_1 = 20$ i = 1,2,3	n <sub>1</sub> = 25 i = 1,2,3	$n_1 = 30$ i = 1,2,3	$n_{i} = 35$ i = 1,2,3
qi	q <sub>1</sub> = .05 i = 1,2,3	q <sub>i</sub> = .05 i = 1,2,3	q <sub>1</sub> = .05 i = 1,2,3	q <sub>i</sub> = .05 i = 1,2,3	$q_{i} = .05$ i = 1,2,3	$q_1 = .05$ i = 1,2,3
CASE NUMBER	57 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	58 α = .05 α = .10 α = .20	59 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	60 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	61 $\alpha$ = .05 $\alpha$ = .10 $\alpha$ = .20	62 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$

Table III (continued)

$^{\sigma}\hat{R}_{L}$	.05242	.05267	.05365	.05065	.05146	.04820
μĥ	.85585 .76698 .80098	.85937 .77062	.85948 .77259	.85617 .7777 .80512	.85775 .7697 .80373	.85405 .77314 .80613
P(R <sub>S</sub> )	.8820	.4070 .8770 .7880	.4350	.4840	.4960 .9120 .7990	.5340
R -A <sub>1-α</sub>	09263 00063 .00353	09384	09501 00720 00397	07394 01024 00630	07598 .01586 00621	07695 .01250 01140
$A_{1-\alpha}$	.9500 .8580 .85385	.95122 .86137 .85811	.95238 .86457 .86135	.93131 .86764 .86367	.93336 .84151 .86358	.93432 .84487 .86878
R S	.85737	.85737	.85737	.85737	.85737	.85737
Σniqi	9.00	6.15	6.30	6.450	9.9	6.75
n,	n; = 40 i = 1,2,3	$n_{\hat{1}} = 41$ i = 1,2,3	$n_1 = 42$ i = 1,2,3	$n_1 = 43$ i = 1,2,3	n; = 44 i = 1,2,3	$n_1 = 45$ 1 = 1,2,3
qi	q <sub>1</sub> = .05 i = 1,2,3	q <sub>i</sub> = .05 i = 1,2,3	$q_1 = .05$ $i = 1, 2, 3$	$q_1 = .05$ $i = 1,2,3$	q <sub>i</sub> = .05 i = 1,2,3	$q_1 = .05$ i = 1,2,3
CASE NUMBER	63 α = .05 α = .10 α = .20	64 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	65 α = .05 α = .10 α = .20	66 α = .05 α = .10 α = .20	67 $\alpha = .05$ $\alpha = .10$ $\alpha = .20$	68 α = .05 α = .10 α = .20

Table III (continued)

o <sub>Ř</sub>	.05161	.0504	.04982	.04794	.0589
u <sub>Ř</sub> ť	.85740 .77464 .80544	.85563 .77991	.85986 .77725	.85830 .77642 .80802	.85591 .77705 .80677
P(R <sub>s</sub> )	.9130 .8140	.4970	.4130	.4500	.4820
R-A <sub>1-α</sub>	07835 .00927 00890	07970 00617	.00320	08223 .00105	06461 00101 00043
$A_{1-\alpha}$	.84810	.93708 .85120	.93837 .85417 .85330	.93961 .85632 .85674	.92198
a s	.85737	.85737	.85737	.85737	.85737
Σniqi	06.90	7.050	7.20	7.35	7.5
ņ	n <sub>i</sub> = 46 i = 1,2,3	$n_1 = 47$ i = 1,2,3	$n_1 = 48$ i = 1,2,3	n <sub>1</sub> = 49 i = 1,2,3	n <sub>i</sub> = 50 i = 1,2,3
qi	q <sub>i</sub> = .05 i = 1,2,3	$q_1 = .05$ $i = 1,2,3$	$q_1 = .05$ $i = 1,2,3$	q <sub>1</sub> = .05 i = 1,2,3	q <sub>i</sub> = .05 i = 1,2,3
CASE NUMBER	$\alpha = .05$ $\alpha = .10$ $\alpha = .20$	$\alpha = .05$ $\alpha = .10$ $\alpha = .20$	$\alpha = .05$ $\alpha = .10$ $\alpha = .20$	$\alpha = .05$ $\alpha = .10$ $\alpha = .20$	α = .05 α = .10 α = .20
CA	69	70	71	72	73

### CHAPTER V

#### CONCLUSIONS

Based upon the results of the simulation, which are tabulated in Tables I through III and illustrated in Figures 3 through 8, the following general conclusions can be drawn:

- a) The accuracy of the method is a function of  $\Sigma n_i q_i$  and, in general, will increase as this value increases. However, the graphs of the accuracy criteria take the shape of a sawtooth curve. Therefore, there is no guarantee that increasing  $\Sigma n_i q_i$  will improve the accuracy of the method. It is generally true, however, that as  $\Sigma n_i q_i$  gets large the difference between system reliability,  $R_s$ , and  $A_{1-\alpha}$  should converge to zero, as should the difference between the desired confidence level,  $(1-\alpha)$ , and  $P(R_s)$ .
- b) At confidence levels of .9 and .8, and for values of  $\Sigma n_i q_i$  which are sufficiently high, the procedure appears to be reasonably accurate. Obviously, the numerical value of "sufficiently high" is subjective and depends upon such unknown parameters as user risk, utility, etc. For most purposes, a value of  $\Sigma n_i q_i \approx 4.0$  should be sufficiently high at both of the above confidence levels. The procedure appears to be inaccurate if  $R_s$  is very high or  $\Sigma n_i q_i$  is small enough to make a failure only moderately probable.
- c) Serious doubt exists as to the acceptability of the method for a confidence level of .95 or greater. At the former two confidence levels there was an apparent convergence toward zero error. No such convergence was apparent at the .95 level.

Even in Cases 6 and 8, where  $\Sigma n_i q_i$  was 22.0 and 23.9, respectively, the difference,  $R_s - A_{1-\alpha}$ , is an order of magnitude greater than the corresponding values for  $\alpha = .1$  and  $\alpha = .2$ . Similarly, the actual confidence level is about half of that intended.

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## APPENDIX I

## GLOSSARY

Meaning	Notation	Computer Simulation Variable Name
System reliability	Rs	RSUBS
Phase reliability	R	RSUBI(I)
System reliability estimator	Î,	RHATS
Phase reliability estimator	$\hat{R}_{ extbf{i}}$	RHATI
Successful tests of the i <sup>th</sup> phase	s	S(I)
Number of tests of the i <sup>th</sup> phase	n i	AN(I)
Estimator for the variance of the reliability estimators	$\hat{\sigma}_{\hat{R}_{\mathbf{s}}^2}$	SIGPSQ
Estimator for the standard deviation of reliability estimators	$\hat{\sigma}_{\hat{R}_{\mathbf{S}}}$	SIG
Computed lower confidence limit	$\hat{R}_{\mathbf{L}}$	RHATL
The $(1-\alpha)^{th}$ percentile of the computed $\hat{R}_L$	A <sub>1-α</sub>	AlA
Probability that $\hat{R}_L$ is less than $R_s$	P(R <sub>s</sub> )	RSPCN
The (i) th percentile of the standard normal distribution	P(i)	P(I)
Mean of the LCL's generated	$^{\mu}\hat{\mathtt{R}}_{\mathtt{L}}$	MEAN
Variance of the LCL's generated	σ <sub>Ř2</sub> L	VAR
Standard deviation of the LCL's generated	σ̂Â <sub>L</sub>	SIGMA
Number of replications per case	KK	KK
Number of phases per case	K	K

### APPENDIX II

#### PROGRAM PRINTOUT

PROGRAM MAIN

PROGRAM MAIN DOES ALL COMPUTATIONS EXCEPT THE COMPUTATION OF THE VALUES RHATS, SYSTEM RELIABILITY ESTIMATOR, AND RHATL, LOWER CONFIDENCE LIMITS. THESE LATTER COMPUTATIONS ARE DONE IN SUBROUTINE RHAT

HERE SET INDEX OF RANDOM NUMBER GENERATOR

XXX=RNG(C)

XXX=RNG(151)

HERE SET ALL SUBSYSTEM PARAMETERS AND TEST STATISTICS TO ZERO TO AVOID CARRYING VALUES OVER FROM ONE CASE STUDY TO THE NEXT.

DO 9 J=1,100 P(J)=0. AN(J) =0. S(J)=0. CONTINUE

HERE READ INTO MEMORY: NUMBER OF REPLICATIONS DESIRED; NUMBER OF SUBSYSTEMS CONSIDERED; ALFA LEVEL; RELIABILITY AND NUMBER OF TESTS FOR EACH SUBSYSTEM.

PEAD(5,900)KK,K,ALFA,( R(J),AN(J), J=1,K)
900 FORMAT (2110, F10.5,/( 2F10.5))

HERE READ INTO MEMORY TEN VALUES OF STAND-ARD DEVIATION OF (1-ALFA) PERCENTILE OF A STANDARD NORMAL DISTRIBUTION.

P(1)=1.645 P(2)=1.2816 P(3)=1.038 P(4)=.8416 P(5)=.675 P(6)=.525 F(7)=.385 P(8)=.253 F(9)=.124 F(10)=.0 RK=KK

HERE INITILIZE THE VALUES OF ALL CUMULATIVE SUMS AND PRODUCTS TO ZERO AND ONE, RESPECTIVELY.

RSUBS=1.
DO 20 J=1,KK
RHATL(J) =C.
CONTINUE
PMU= 0.
SUM= 0.
SUMA = 0.

000000

CCCCCC

0000000

CCCCCC

С

HERE COMPUTE SYSTEM RELIABILITY, THAT IS THE PRODUCT OF ALL SUBSYSTEM RELIABILITIES. CCC PO 5C IZ=1,K RSUBS=RSUBS\*R(IZ) CONTINUE 50 0000000 HERE COMPUTE THE SUM OF PRODUCTS (N(I) X Q(I)), THE AMOUNT OF TESTING TIMES THE SUBSYSTEM UNRELIABILITY, FOR ALL SUBSYSTEMS. DO 45C JR=1,K SUMA = (AN(JR)\*(1.-CONTINUE R(JR)))+SUMA 450 CCCCC HERE BEGIN GATHERING TEST DATA FOR EACH OF KK REPLICATIONS. DO 100 IX=1,KK 000000 HERE SET THE VALUE S(4), THE NUMBER OF SUCCESSFUL TRIALS, TO ZERO FOR EACH SUSYSTEM. BEGIN TESTING. SUB-CO 10 J=1,K S(J)=0. CONTINUE DO 20C IA=1,K NIA=AN(IA) DO 2CO IB=1,NIA CCCCCCCCC HERE COMPARE AN(IA) RANDOM NUMBERS TO RELIABILITY OF THE (IA)TH SUBSYSTEM, AN(IA) BEING THE NUMBER OF TESTS DESIRED FOR THE (IA)TH SUBSYSTEM. IF THE RANDOM NUMBER IS EQUAL TO OR LESS THAN SUBSYSTEM RELIABILITY A SUCCESSFUL TEST IS COUNTED. IF ( R(IA)-RNG(1)) 200,199,199
S(IA)=S(IA)+1.
CONTINUE 199 200 HERE CALL SUBROUTINE 'RHAT' WHICH COMPUTES
THE LOWER CONFIDENCE LIMIT FOR THE TEST
STATISTICS GATHERED ABOVE. THE LOWER CONFIDENCE LIMIT IS RETURNED AND STORED IN
TWO DIFFERENT VECTOR MATRICES 'RHATL' AND
'A1' FOR FURTHER COMPUTATIONS. THEY ARE
ALSO SUMMED FOR LATER COMPUTATION OF THEIR MEAN
SUBROUTINE 'RHAT' ALSO RETURNS KK VALUES
OF THE SYSTEM RELIABILITY ESTIMATOR 'RHATS'.
THESE VALUES ARE ALSO STORED IN A VECTOR
MATRIX FOR LATER PRINTOUT. CALL RHAT (ALFA, PHIH, CAPA)
RHATL(IX) = PHIH
RHATS(IX) = CAPA
A1(IX) = RHATL(IX)
PMU = PMU + RHATL(IX)
CONTINUE 100 C

HERE THE LOWER CONFIDENCE LIMIT MATRIX AND THE SYSTEM RELIABILITY ESTIMATOR MATRIX ARE SORTED INTO ASCENDING ORDER OF THEIR CCCCC VALUES. CALL SHSORT(A1,A2,KK)
CALL SHSORT(RHATS,CAP1,KK) 000000 HERE DIVIDE ACCUMULATED SUMS OF LOWER CON-FIDENCE LIMITS BY THE NUMBER OF REPLICA-TIONS TO COMPUTE THEIR MEAN. MEAN=PMU/BK 000000000 HERE COMPUTE THE VALUE 'KALFA' THAT IS
( 1 - ALFA ) X THE NUMBER OF REPLICATIONS.
THIS VALUE IS USED AS THE INDEX NUMBER OF
THE ORDERED LOWER CONFIDENCE LIMIT MATRIX.
THUS A1(KALFA) IS THE (1-ALFA)TH PERCENTILE
OF THE LOWER CONFIDENCE LIMIT DISTRIBUTION. AALFA=(1.-ALFA)\*BK KALFA=AALFA A1A=A1(KALFA) CCCCCC HERE COMPUTE THE PERCENTILE ASSOCIATED WITH R SUB S IN A WAY SIMILAR TO THE METHOD DESCRIBED ABOVE. RST=RSUBS DO 4GC IC=1,KK IF(RST-A1(IC)) 398,399,399 KIC=IC-1 FIC=KIC RSPCN =PIC/BK RST=1.1 398 CCCCC HERE COMPUTE VARIANCE AND STANDARD DEVI-ATION OF THE LOWER CONFIDENCE LIMIT DISTRIBUTION. 399 NUM=RHATL(IC)-MEAN NUMSQ=NUM\*NUM SUM=SUM+NUMSQ CONTINUE 400 VAR = SUM/BK SIGMA = SORT(VAR) CCCC HERE COMPUTE THE VALUE RSUBS - A SUB(1-ALFA). DIFF = RSUBS-A1A CCCC HERE PRINT OUT ALL DESIRED VALUES AND RESULTS. WRITE(6,101C)
WRITE(6,1011)(J,AN(J), R(J),J=1,K)
WRITE(6,1002)RSUBS
WRITE(6,1003)A1A
WRITE(6,1004)SIGMA
WRITE(6,1005)RSPCN
WRITE(6,1006)MEAN
WRITE(6,1023)DIFF
WRITE(6,1024)SUMA

1023 FORMAT(////10x,'R SUB S - A SUB(1-ALFA) EQUALS',
\*F15.5)
1024 FORMAT(////10x,'SIGMA (N(I) X O(I)) EQUALS',F15.5)
1010 FORMAT(1H1,38X,'I',12X,'N(I)', 9X,'R(I)'//)

```
1011 FORMAT(38X, I2, F15.0, F15.3)
1001 FORMAT (////(10X, 5F15.5))
1002 FORMAT (////10X, R SUB S (SYSTEM RELIABILITY)*,

*'EQUALS*, F15.5)
1003 FORMAT (////10X, '(1-ALFA) X 100 PERCENTILE ',

*'(A SUB 1 - ALFA) EQUALS ', F15.5)
1004 FORMAT (////10X, 'STANDARD DEVIATION OF COMPUTED ',

*'LOMER CONFIDENCE LIMIT EQUALS', F15.5)
1005 FORMAT (////10X, 'PERCENTILE ASSOCIATED WITH '

*'R SUB S EQUALS', F15.5)
1006 FORMAT(////10X, 'MEAN OF COMPUTED LOWER CONFIDENCE',

*'LIMIT EQUALS', F15.5)
1020 FORMAT(10X, '100C VALUES OF THE LOWER CONFIDENCE',

*'LIMIT, LISTED IN ACCENDING ORDER CONFIDENCE',

*'LIMIT, LISTED IN THE ORDER GENERATED')
1022 FORMAT(10X, '100C VALUES OF THE ESTIMATOR FOR THE',

*'SYSTEM RELIABILITY (RHATS)')

WRITE(6,10C1)A1

WRITE(6,10C1)A1

WRITE(6,10C1)RHATL

WRITE(6,10C1)RHATL

WRITE(6,10C2)

WRITE(6,10C1)RHATL

WRITE(6,10C2)

WRITE(6,10C1)RHATS

STOP
END
```

### SUBROUTINE RHAT

SUBROUTINE RHAT COMPUTES THE VALUES RHATS (SYSTEM RELIABILITY ESTIMATOR) AND RHATL (LOWER CONFIDENCE LIMIT) USING AS ITS CALLING PARAMETERS THE STATISTICS GENERATED IN PROGRAM MAIN. IT IS A STRAIGHTFORWARD APPLICATION OF THE APPLIED PHYSICS LAB-

COMMON R(10C), AN(100), S(100), PHATL(1000), F(10), \*A1(1000), A2(1000), KK, K

HERE INITIALIZE VALUES AS NECESSARY

PIPSO=1. PROD=1. CAPP=1.

CCCC

CCCC

CCCCC

00000000

CCCCCC

00000

HERE "RHATI" IS SYBSYSTEM RELIABILITY ESTIMATOR

DO 50C JA=1,K RHATI=S(JA)/AN(JA) FSQ=RHATI\*RHATI

HERE PIPSO IS THE PRODUCT OF THE SQUARED SUBSYSTEM ESTIMATORS.

PIPSQ=PIPSQ\*PSQ

THE PURPOSE OF THIS STATEMENT IS TO PRE-VENT EXPONENT UNDERRUN, THAT IS, IT PRE-VENTS NUMBERS FROM GETTING SMALLER THAN THE COMPUTER CAN EFFECTIVELY HANDLE. IT SETS VERY SMALL NUMBERS EQUAL TO ZERO.

IF(PIPSQ-.00C000C1)501,502,502
501 PIPSQ=0.
PROD=0.

THIS STATEMENT IS A CODIFICATION OF THE SECOND TERM OF THE RIGHT HAND SIDE OF EQUATION (5), CHAPTER II.

5C2 PROD=PROD\*(PSQ-(RHATI\*(1.-RHATI)) /(AN(JA)-1.))
CAPP=CAPP\*RHATI
500 CONTINUE

THIS STATEMENT IS A CODIFICATION OF THE ENTIRE EQUATION (5), CHAPTER II.

SIGPSO=PIPSO-PROD SIGP=SQRT(SIGPSQ) BALFA=ALF +20. JALFA=BALFA

HERE COMPUTE THE VALUE OF THE LOWER CONFIDENCE LIMIT, CALLED PHA IN THIS SUBROUTINE.

PHA =CAPP-(P(JALFA)\*SIGP)
RETURN

CCCCC

## SUBROUTINE SHSORT

```
SUBROUTINE SHSORT(A, KEY, /N/)

DIMENSION A(N), KEY(N)

M1=1
6 M1=M1*2
IF(M1-N) 6,6,8
8 M1=M1/2-1
MM=MAXO(M1/2,1)
GO TO 21
2C MM=MM/2
IF(MM)100,100,21
21 K=N-MM
22 DO 1 J=1,K
II=J
11 IM=II+MM
IF(A(IM)-A(II)) 30,1,1
3C TEMP=A(II)
A(II)=A(IM)
KEY(II)=KEY(IM)
A(IM)=TEMP
KEY(IM)=IT
II=II-MM
IF(II) 1,1,11
1 CONTINUE
GO TO 20
100 RETURN
END
```

## FUNCTION SUBROUTINE RNG

FUNCTION RNG(N)
NR=N
IF(NR)10,10,20
10 IX=30517
NR=NR+1
20 DO 50 I=1,NR
IY=IX\*65539
IF(IY)5,6,6
5 IY=IY+2147483647+1
6 RNG=IY
RNG=RNG\*.4656613E-9
IX=IY
RETURN
END

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Systems which are composed of two or more phases, or subsystems, arranged in logical sequence are found frequently in industry and defense. Standard procedures for computing lower confidence limits on reliability of such systems rely on the use of system data. Engineering changes to any of these subystems can effect the invalidation of all existing data, necessitating additional, sometimes extensive, testing. Such changes are not infrequent in complex systems. A need exists for a method of computing lower confidence limits on reliability which uses phase data. Some approximation techniques have become available. One such technique is currently being used by Applied Physics Laboratory, The Johns Hopkins University. Computer simulation techniques are used to analyze the accuracy of this procedure.

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